

1 **Spectral Analysis of Surface Waves Scanning to Identify Debonding Conditions between**  
2 **HMA Layers in Pavements**

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38 **ABSTRACT**

39 This paper presents a recently developed system used for condition assessment of hot mix  
40 asphalt (HMA) pavements to detect debonding between layers of HMA pavements. The study  
41 was partly funded by the Strategic Highway Research Program 2 (SHRP 2) - R06D research  
42 project titled “Nondestructive Testing to Identify Delaminations between HMA Layers” through  
43 the National Center for Asphalt Technologies (NCAT). The objective of the study was to  
44 develop a reliable technique to determine internal condition of HMA pavements including  
45 debonding conditions between each layer. An Impact Echo and Spectral Analysis of Surface  
46 Waves Scanner (IE/SASW Scanner) prototype (originally developed for condition assessment of  
47 bridge decks) with up to three pairs of transducer wheels using Spectral Analysis of Surface  
48 Waves scanning was employed in this project. This paper includes background of the  
49 development of the IE/SASW Scanner and a case study performed on HMA pavements of  
50 known conditions at the NCAT Pavement Test Track. The research investigation was performed  
51 as a “blind” study, with the actual known pavement conditions revealed to the research team  
52 after initial data analysis and reporting of detected delamination conditions was completed.

53

**54 INTRODUCTION**

55 The bonding condition between layers of HMA pavements is an important issue regarding long  
56 term performance for multi-layered pavement structures. Good bonding conditions between  
57 layers will lead to a longer service life of multi-layer HMA pavements (1 and 2). Development  
58 of reliable, non-destructive evaluation techniques that can accurately identify locations and  
59 depths of debonding are critical. Identification of these defects allows agencies to repair the  
60 discontinuity before affecting the long term safety and service life of the pavement. This paper  
61 includes the background of the IE/SASW Scanning system development and a blind case study  
62 investigation on HMA pavements of known conditions.

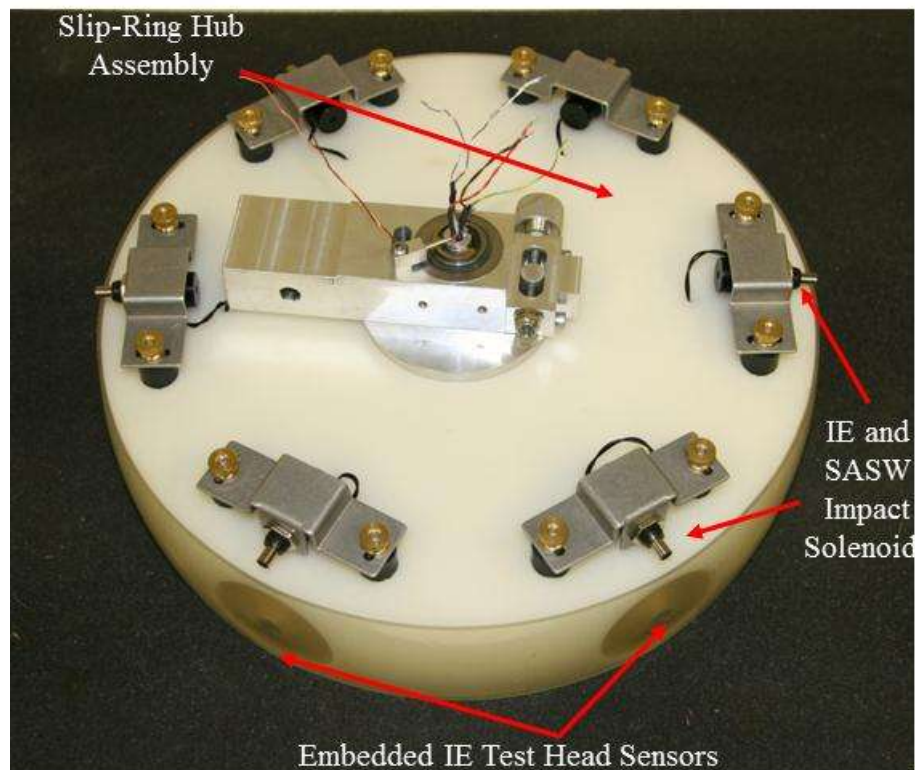
**63 BRIEF BACKGROUND OF THE SPECTRAL ANALYSIS OF SURFACE WAVES  
64 TECHNIQUE**

65 The Spectral Analysis of Surface Waves (SASW) method is typically applied to structural  
66 elements to estimate surface-opening crack depths, fire damage and freeze-thaw damage depths,  
67 and the measure relative concrete quality. It can also be used for thickness profiling of  
68 pavements, including asphalt and layer systems. The method uses the dispersive characteristics  
69 of surface waves to determine the variation of the shear wave velocity (stiffness) of layered  
70 systems with depth. Aouad et al. described the theory of the SASW test in details (6). Surface  
71 opening cracks, honeycomb zones, fire damage, and other flaws with create an effective "layer"  
72 of low velocity material with a depth which can be measured. In general once the shear wave  
73 velocity profiles are determined, shear and Young's moduli of the materials can also be  
74 estimated through the use of simple mathematical equations. The shear wave velocity profiles  
75 (shear wave velocity versus depth) are determined from the experimental dispersion curves  
76 (surface wave velocity versus wavelength) obtained from SASW measurements through a  
77 process called forward modeling or through an inversion process. The shear wave velocity  
78 measurements can be used to compare concrete areas to locate zones of weak or degraded  
79 concrete. In this project, the shear wave velocities were not calculated and only the surface wave  
80 velocities at different depths were used as an indication for pavement debondings. The SASW  
81 method can be performed on any material provided there is an accessible surface for receiver  
82 attachments and source impacting.

**83 IMPACT ECHO/SPECTRAL ANALYSIS OF SURFACE WAVES SCANNER (IE/SASW  
84 SCANNER)**

85 The IE/SASW Scanner was recently developed by the research team at Olson Engineering as  
86 part of research funded by the National Cooperative Highways Research Program – Innovations  
87 Deserving Exploratory Analysis program (3). The system was originally developed for rapid  
88 condition assessment of bridge decks using a pair of transducer wheels, and thus the name  
89 "Bridge Deck Scanner (BDS)". As part of the research project funded by the SHRP 2 (R06D)  
90 research program through NCAT, the system was later expanded to up to three sets of identical  
91 transducer wheels to allow for more rapid testing. The name of the system was changed to  
92 Impact Echo/Spectral Analysis of Surface Waves Scanner (IE/SASW Scanner) to make it more  
93 generalized to both bridge and pavement applications. Figure 1 shows a transducer wheel  
94 assembly. The transducer wheel was designed to include six piezo-ceramic displacement

95 transducers at 6 inch (152.4 mm) spacings, resulting in a wheel circumference of 3 feet (0.91  
 96 meter) or a diameter of approximately 11.5 inches (279.4 mm). The 6 inch (152.4 mm)  
 97 transducer spacing was utilized to provide relatively close measurement intervals consistent with  
 98 a high data resolution bridge deck survey. The six transducers incorporated into each wheel are  
 99 spring mounted with rubber isolators and captured with a thin replaceable urethane tire  
 100 approximately 2.5 inches (63.5 mm) wide. The thin urethane tire was added as a dust cover to  
 101 prevent dirt from entering the sensor housing and, more importantly, to increase sensor contact  
 102 area and improve sensor coupling. The transducer wheel design of the IE/SASW Scanner uses a  
 103 solenoid impactor to impart energy into the material surface, creating high amplitude signals  
 104 which are easily measured by the transducer. The solenoids were mounted to the side of the  
 105 rolling transducer wheel in line with the sensor element, thus ensuring the solenoid height  
 106 (distance between material surface and solenoid) remained constant to improve test consistency.  
 107 The urethane tire, large impacting solenoids, and overall sensor weight (approximately 25 lbs or  
 108 11.3 kilogram), which affects contact pressure, are the primary improvements over the rough  
 109 surface performance of the BDS system.



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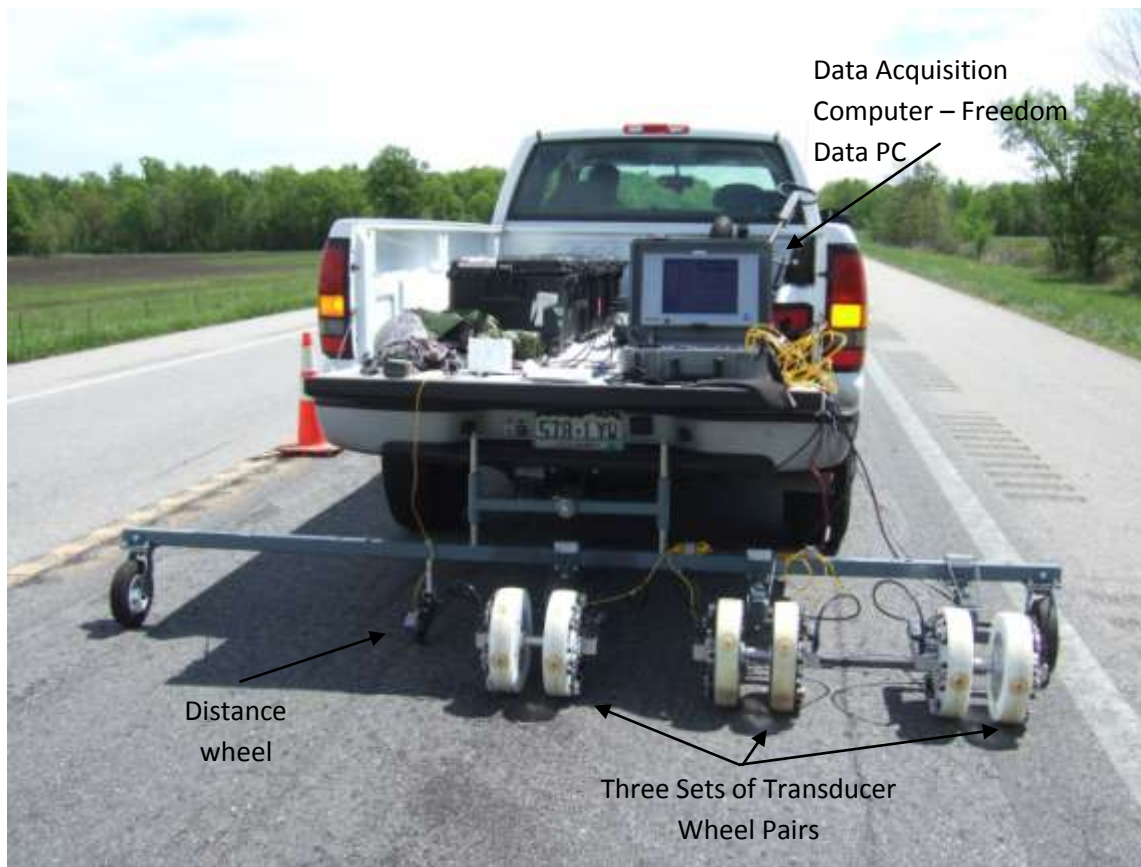
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**Figure 1 – Transducer Wheel Assembly**

112 Two identical transducer wheels constitute a “set”, which work in concert with one another  
 113 during testing. The IE/SASW Scanner can be equipped with up to three sets of transducer  
 114 wheels. The system can be easily attached to either a vehicle hitch as shown in Figure 2 with  
 115 three sets of transducers, or a scanning cart when only one set of transducer wheels are used.

116 The IE/SASW Scanner can perform:

- 117 1) Impact Echo tests on each transducer wheel simultaneously with the transducer and  
 118 impactor on adjacent wheels offset to avoid signal interference. This set-up is ideal for  
 119 condition assessment of bare concrete decks if top delamination and general integrity are  
 120 the primary concern. The spacing between the two adjacent transducer wheels can be set  
 121 between 6 inches (0.15 meter) and 2 feet (0.61 meter) depending on the desired scan  
 122 resolution.
- 123 2) Impact Echo and Spectral Analysis of Surface Waves can be scanned simultaneously by  
 124 aligning the transducer elements of both transducer wheels within a “set”. The first  
 125 transducer wheel (with the impactors activated) collects IE data as well as the first  
 126 channel of SASW data. The second wheel (with the impactors off) collects the second  
 127 channel of SASW data. Both IE and SASW tests can be performed simultaneously in a  
 128 single scan. This setup provides additional information for assessment of complex  
 129 pavement structures such as layered HMA or concrete decks with asphalt overlays,  
 130 which, in past experience, have been problematic for IE testing alone.



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132 **Figure 2: Current IE/SASW Scanning System, showing the SASW test set-up of 6 inch**  
 133 **(152.4 mm) transducer spacings with a distance of 2 feet (0.61 meter) between pairs on**  
 134 **HMA Pavement.**

135

136 **CASE STUDY: IE/SASW SCANNING ON A HMA PAVEMENT AT NCAT SITE**

## 137 **Project Background**

138 The main objective of the SHRP 2 Project R06(D) is to identify and develop rapid  
139 nondestructive testing (NDT) techniques with 100 percent continuous coverage that are capable  
140 of identifying and determining the extent and depth of delaminations and discontinuities in HMA  
141 pavements. The IE/SASW Scanner developed by Olson Engineering was one of the technologies  
142 that NCAT evaluated. During early stages of the research the hardware and software of the  
143 IE/SASW Scanning system was expanded to allow connection of up to three sets of transducer  
144 wheels to widen the testing field for actual real world pavement testing scenarios. The system  
145 was then evaluated in a “blind” research study to measure the known HMA pavement conditions  
146 at the NCAT Pavement Test Track. The known pavement conditions were not revealed to the  
147 researchers until after data analysis and reporting of results was completed.

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## 150 **Construction of Pavement Test Sections at the NCAT Pavement Test Track**

151 NCAT constructed ten test sections at the NCAT test track facility located near Auburn, AL.  
152 Pavement conditions ranging from complete debonding to good bonding were simulated at the  
153 interfaces between dense-graded asphalt layers. Good bonding conditions were ensured by using  
154 a tack coat, while poor bonding conditions were constructed by using bond breakers such as  
155 baghouse fines and multiple layers of heavy craft paper between asphalt lifts. In addition, a 25.4  
156 mm (1 inch) thick un-compacted coarse fractionated RAP material was used to simulate a  
157 “stripping” condition. Each test section is 25 feet (7.62 meter) in length and 12 feet (3.66 meter)  
158 in width.

## 159 **IE/SASW Scanning for Multi-Layers HMA Pavements to Detect Bonding Conditions**

160 An IE/SASW Scanner using the SASW measurement equipment setup was used to assess the  
161 condition of the test sections. For this setup, the solenoid impactors were activated for one  
162 transducer wheel and off for the second transducer wheel. This setup allows the Impact Echo  
163 Scanning and Spectral Analysis of Surface Wave Scanning to be performed simultaneously in a  
164 single scan. The SASW data gave clear indications of bonding conditions and the IE data were  
165 also used in the analysis as a comparison. The background and theory of the SASW test method  
166 can be found in many publications (5 and 6).

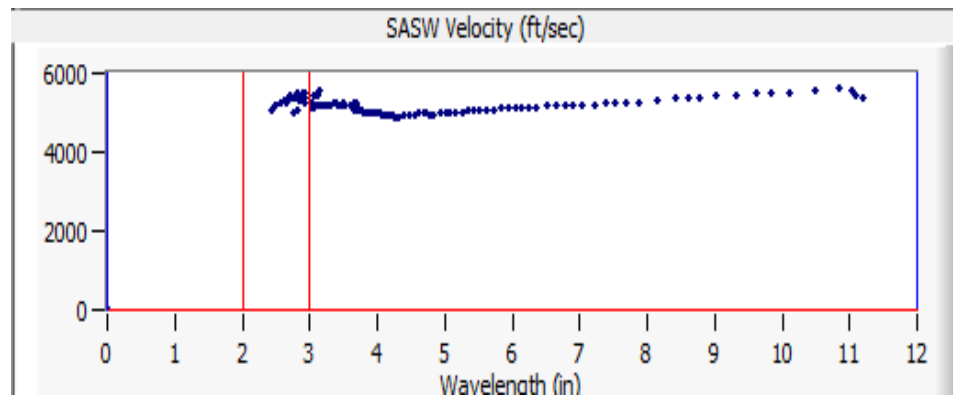
## 167 **SASW Data Interpretation**

168 Sound pavements typically yield a high and relatively constant surface wave velocity observed  
169 as a flat, horizontal line in the dispersion curve throughout the depth of the pavement. A typical  
170 example of a “Sound” pavement condition is shown in Figure 3. The presence of a sharp drop in  
171 the dispersion curve (surface wave velocity vs wavelength or depth) was found to be a reliable  
172 indication of debonding between layers of HMA pavements. The depth or wavelength of the  
173 velocity drop directly relates to the depth of the debonding. Figure 4 presents a dispersion curve  
174 from a location from Section 1 from the NCAT test track. The actual as-built plan at this test  
175 location showed baghouse dust at a depth of 5 inches (127 mm) to simulate a debonding  
176 conditions between the HMA lift and underlying concrete. Review of Figure 4 shows a sharp

177 drop in the surface wave velocity at a depth of 5 inches (125 mm), which agreed with poor  
 178 bonding at the depth of the HMA layer boundary with simulated debonding. Figure 5 presents a  
 179 dispersive curve from a location from Section 6 from the NCAT test track. The actual as-built  
 180 plan at this test location showed stripping between depths of 2 inches (50.8 mm) HMA surface  
 181 lift and 3 inches (76.2 mm) HMA leveling lift. Review of Figure 5 shows a sharp drop in the  
 182 surface wave velocity at a depth of 3 inches (76.2 mm), which agreed with the approximate  
 183 stripping depths at that location.

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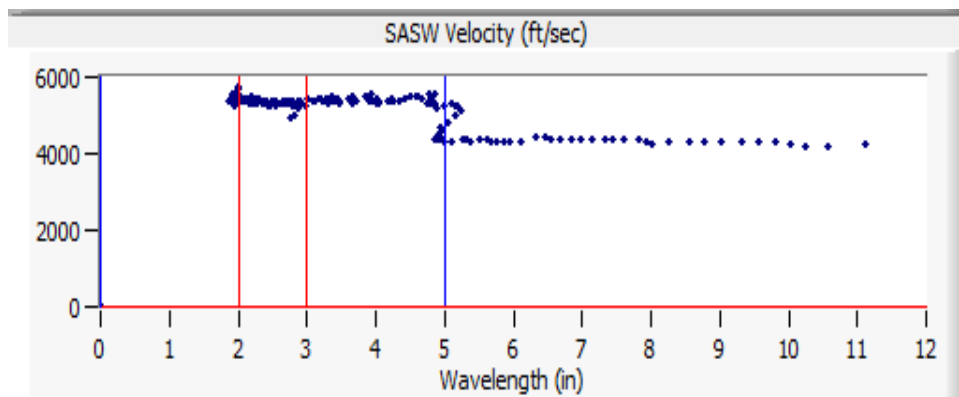
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191 **Figure 3 – A Dispersion Curve from a Sound Location on NCAT Pavement**

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200 **Figure 4 – A Dispersion Curve from a Location from Section 1 with Debonding at a Depth**  
 201 **of 5 inches (127 mm)– Note Drop in Velocity at Approximately the Same Wavelength**  
 202 **(Depth)**

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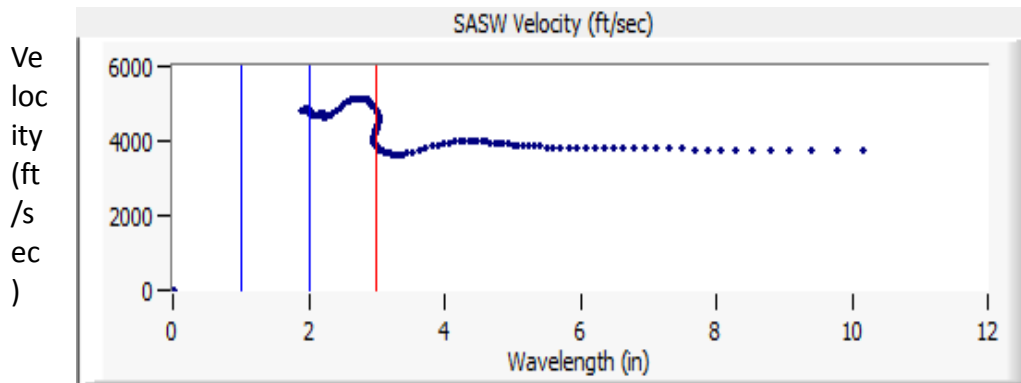
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217 **Figure 5 – A Dispersion Curve from a Location from Section 6 where Simulated Stripping**  
 218 **between Depths of 2 inches (50.8 mm) HMA surface lift and 3 inches (76.2 mm) HMA**  
 219 **leveling lift Note Drop in Velocity at Approximately the Same Wavelength (Depth)**

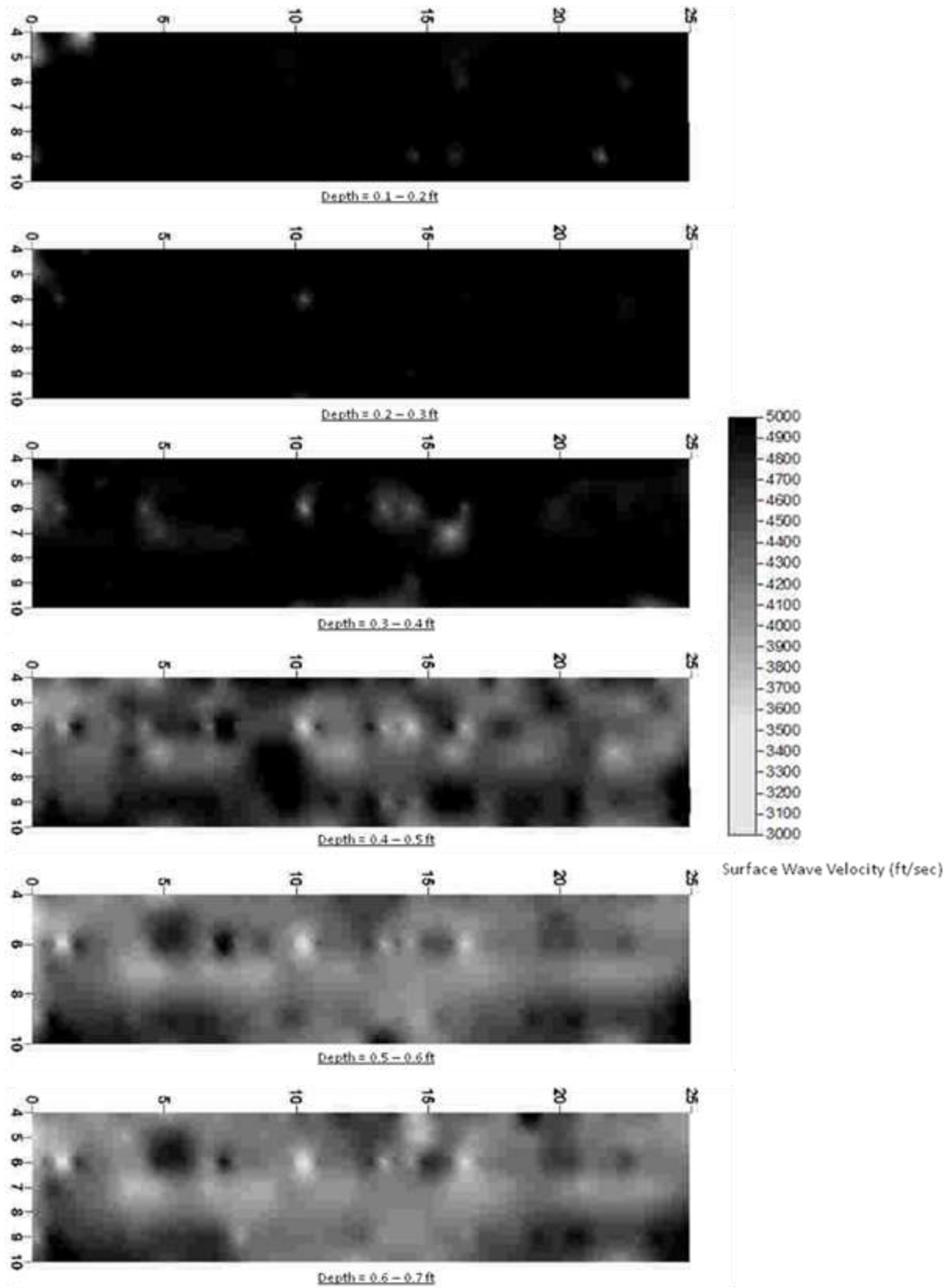
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### 221 Test Results from the IE/SASW Scanner – SASW Scanning Component

222 The test results are presented as plan view images of the test area with the grayscale  
 223 representing the average surface wave velocity at a particular depth range. Multiple plots are  
 224 presented to cover depths from 0.1 to 0.8 feet (30 to 244 mm) from the surface. Surface wave  
 225 velocities are presented in a grayscale ranging from 3,000 ft/sec (914 m/s) - shown in light gray  
 226 color to 5,000 ft/sec (1,524 m/s) - shown in black color. The higher the surface wave velocity,  
 227 the better the condition of the asphalt pavement. Anomalies are revealed as light colored spots or  
 228 areas, where the velocities are lower than normal conditions. Creating multiple plots by  
 229 representing slices of data at different depth ranges allows the depth of anomalies to be  
 230 determined. Figures 6 to 8 present the surface wave velocity profiles from three out of ten  
 231 sections of the NCAT Pavement Test Track. Note that the test results from all ten sections  
 232 represented the actual conditions of the test track relatively well. However, only the test results  
 233 from the clearest three sections are presented herein.

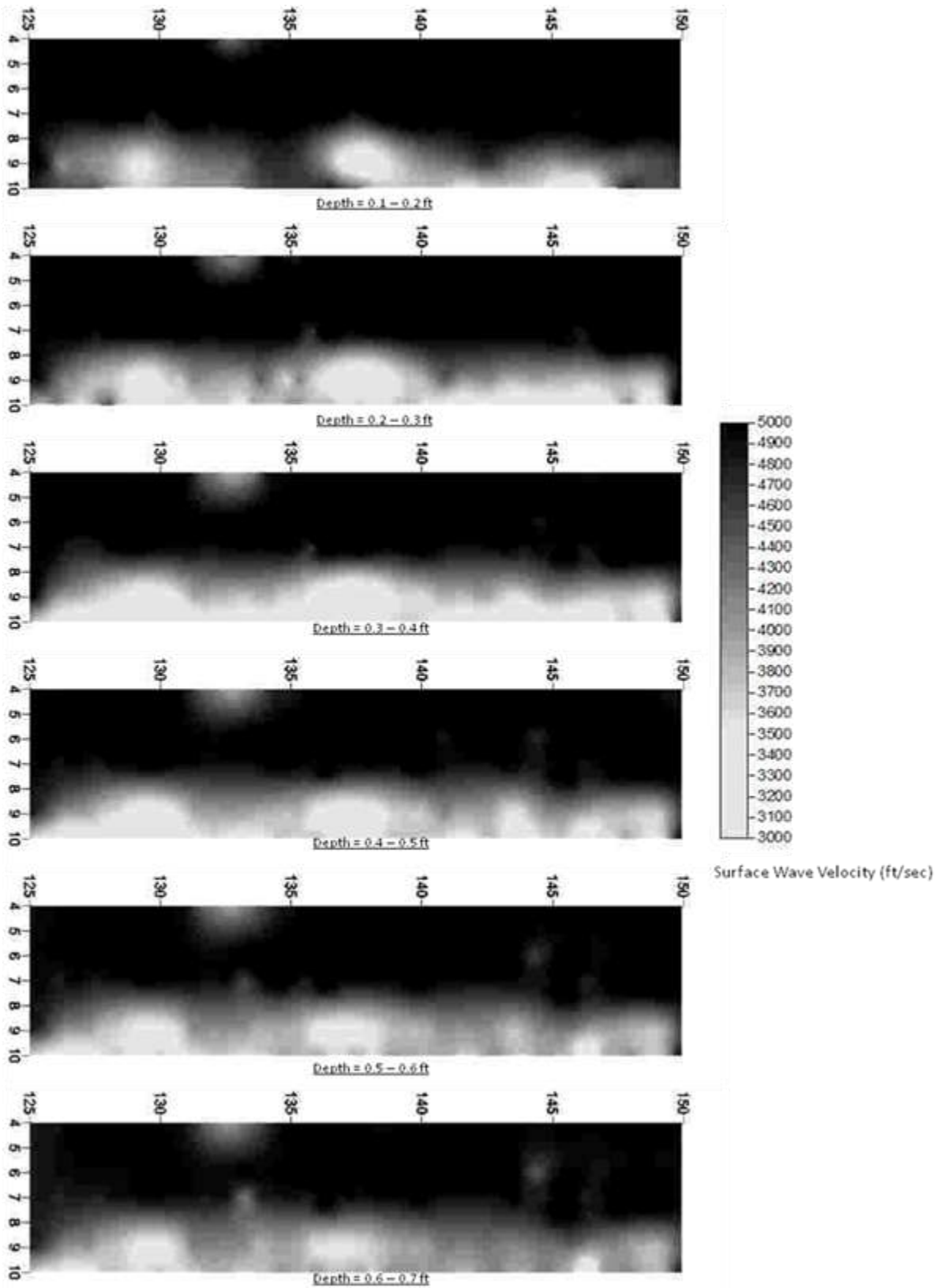
234 Reviews of Figure 6 (Section 1) show a significant drop of surface wave velocities indicating  
 235 likely debonding between depths of 4.8 and 6 inches or 0.4 and 0.5 ft (121.9 and 152.4 mm).  
 236 Reviews of Figure 7 (Section 6) show low velocities from measurement Grid Lines 9 and 10 at  
 237 the shallow depth of 1.2 – 2.4 inches or 0.1 – 0.2 ft (30.5 – 60.96 mm). This is indicative of  
 238 debonding at depths between 1.2 and 2.4 inches or 0.1 and 0.2 ft (30.5 – 60.96 mm). Last,  
 239 reviews of Figure 8 (Section 7) show that the surface wave velocities are relatively constant  
 240 throughout the depths indicative of sound pavements except at the lower left corner (a few test  
 241 locations) where the test results show a shallow delamination between 1.2 and 2.4 inches or 0.1  
 242 and 0.2 ft (30.5 – 60.96 mm).





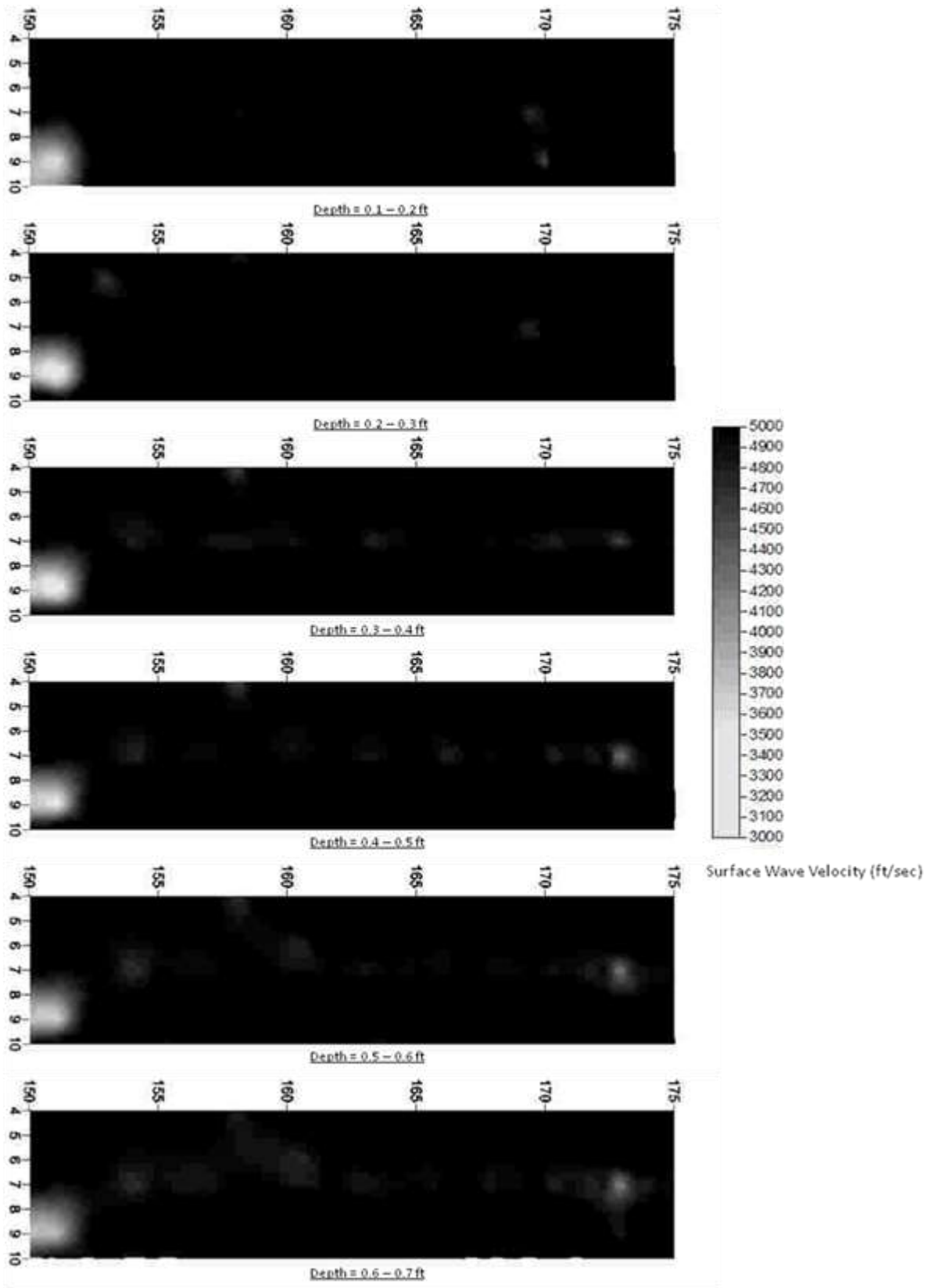
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244 **Figure 6 – Profile (Depth) Plot of Surface Wave Velocities from Section 1**



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246 **Figure 7 – Profile (Depth) Plot of Surface Wave Velocities from Section 6**



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248 **Figure 8 – Profile (Depth) Plot of Surface Wave Velocities from Section 7**

249 **Discussion of Test Results and Comparisons between the SASW Test Results and Actual**  
250 **Conditions**

251 The known as-built conditions of Sections 1, 6 and 7 are summarized below:

- 252 • Section 1 – There is no bond between 5 inches or 0.42 feet (127 mm) of HMA  
253 overlay and the concrete pavement throughout the whole section. Baghouse dust was  
254 used as the bond breaker for half of the width of the section and paper was used on  
255 the other half.
- 256 • Section 6 - Simulated stripping in the wheel path between 1.92 inches or 0.16 feet  
257 (50.8 mm) HMA surface lift and 3 inches or 0.25 feet (76.2 mm) HMA leveling lift.
- 258 • Section 7 - Good bond between 5 inches or 0.42 feet (127 mm) HMA overlay and  
259 HMA pavement except one corner of the section (lower left side) had extended  
260 simulated stripping condition from Section 6.

261 The test results in Figure 6 (Section 1) indicate likely debonding between depths of 4.8 and 6  
262 inches or 0.4 and 0.5 ft (121.9 and 152.4 mm). The interpretation of the SASW test results agree  
263 well with the as built condition of Section 1. The test results in Figure 7 (Section 6) indicate  
264 debonding from measurement Grid Lines 9 and 10 at the shallow depth of 1.2 – 2.4 inches or 0.1  
265 – 0.2 ft (30.5 – 60.96 mm). The SASW test results also agree well with the actual built in  
266 condition of Section 6. Last, the test results of Figure 8 (Section 7) are indicative of sound  
267 pavements except at the lower left corner (a few test locations) where the test results show a  
268 shallow delamination between 1.2 and 2.4 inches or 0.1 and 0.2 ft (30.5 – 60.96 mm). This  
269 finding again agrees well with the as-built conditions of Section 7 where the majority of the  
270 section is sound except one corner where the stripping condition was accidentally extended from  
271 Section 6.

272 **CONCLUSIONS**

273

274 The Spectral Analysis of Surface Waves method can be effectively used to identify the bonding  
275 conditions of multi-layer HMA pavements. The IE/SASW Scanner accelerates the testing  
276 process by allowing up to three scan lines to be tested at once in a rolling system traveling  
277 approximately 1 mph. The system can be attached to either a vehicle or a hand cart. An  
278 important finding from the research project was the determination that a significant drop in the  
279 surface wave velocity in the dispersion curve is a good indication of debonding between layers  
280 of HMA pavement layers. The dispersion curve also indicates the approximate depth at which  
281 the debonding occurs, which is valuable information for assessing repair alternatives.  
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